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4

1819.09m

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1				31 24 48.52	104 47 31.14
				31 24 42.24	104 47 39.58
				31 24 34.67	104 47 32.24
				31 24 50.18	104 47 47.23
				31 24 35.76	104 47 47.46
				31 24 42.92	104 47 56.29
				31 24 42.24	104 47 39.58
				31 24 29.85	104 47 52.99

□

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(%)		97						97
		0.85		+0.15				1
%	90	92				+2	92	94
(%)	92	92					92	92
(%)		97						97

□ □







•”• ] Q ù ,pP€õA Đ



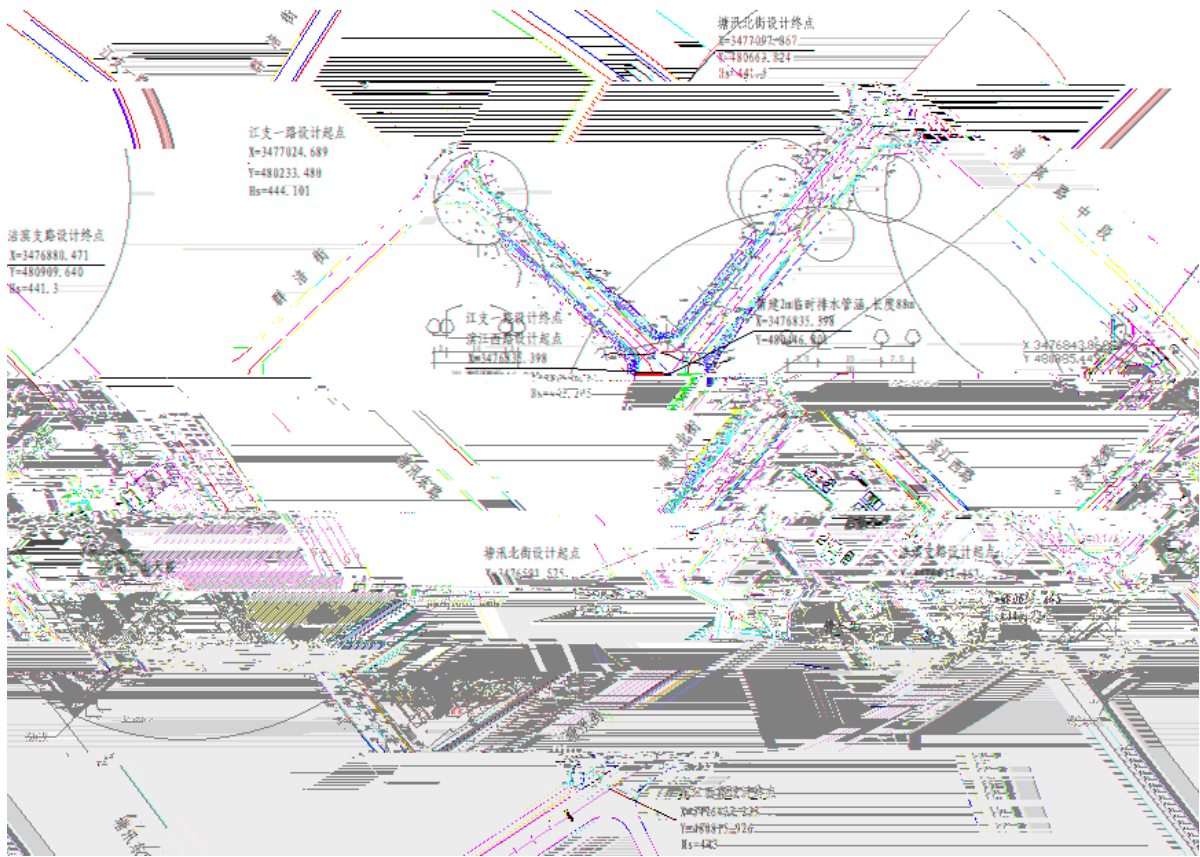
	4.53hm <sup>2</sup> 1819m		11000	( ) 6829.49
	2024 5		2025 2	2025
hm <sup>2</sup>	4.76	hm <sup>2</sup>	4.53	hm <sup>2</sup> 0.23
	m <sup>3</sup> )			
		7.95	17.05	9.10 /
				/
	hm <sup>2</sup> )	4.76	[t/(km <sup>2</sup> .a)]	500
	t)	155.49	t)	143.58
	%)	97		1
	%)	94	%)	92
	%)	97	%)	25
	<b>0.45m<sup>3</sup></b> <b>0.45 m<sup>3</sup></b> <b>3139m</b> <b>86</b> <b>10709m<sup>2</sup></b> <b>3326m</b>		<b>317</b> <b>11484m<sup>2</sup></b>	27207m <sup>2</sup> 3326m 5 <b>1</b>
	0.23 hm <sup>2</sup>		0.23hm <sup>2</sup>	2300m <sup>2</sup> 114m 2 68m
	371.95		223.57	37.26
	752.36			77.86
	/		23.66	6.19
	17			76
	621000			621000
	/15608250018			/13990133013
	1461616224@qq.com			

□

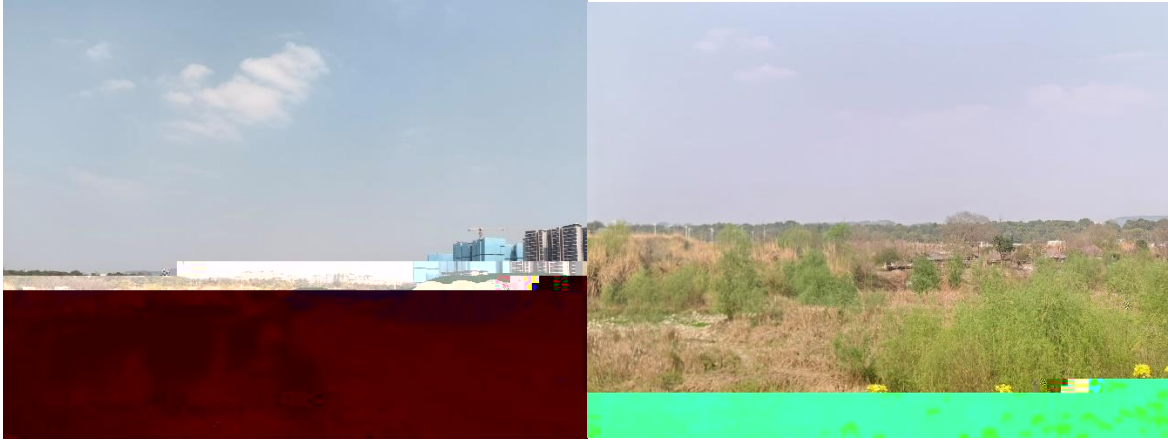
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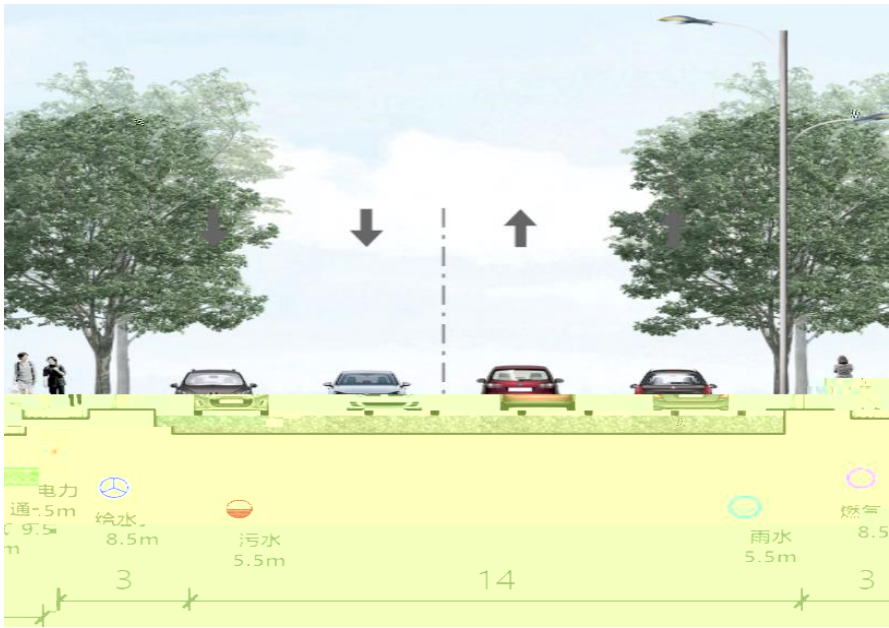
□

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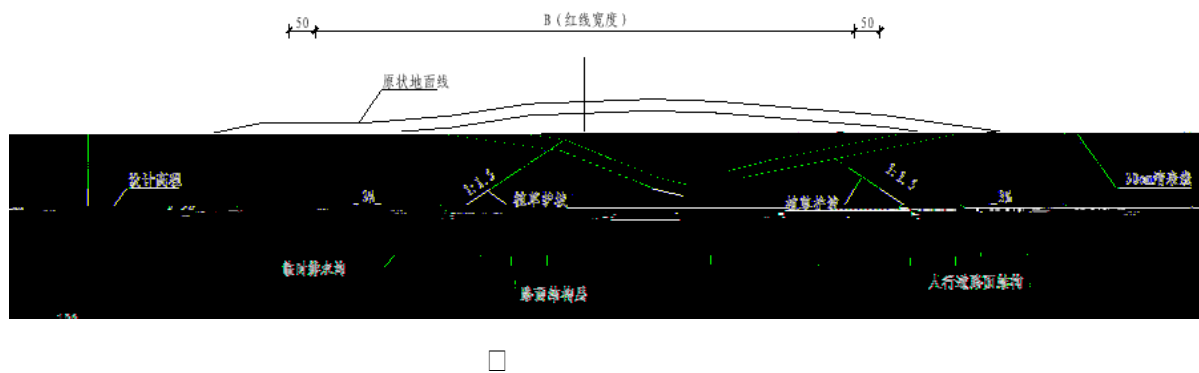
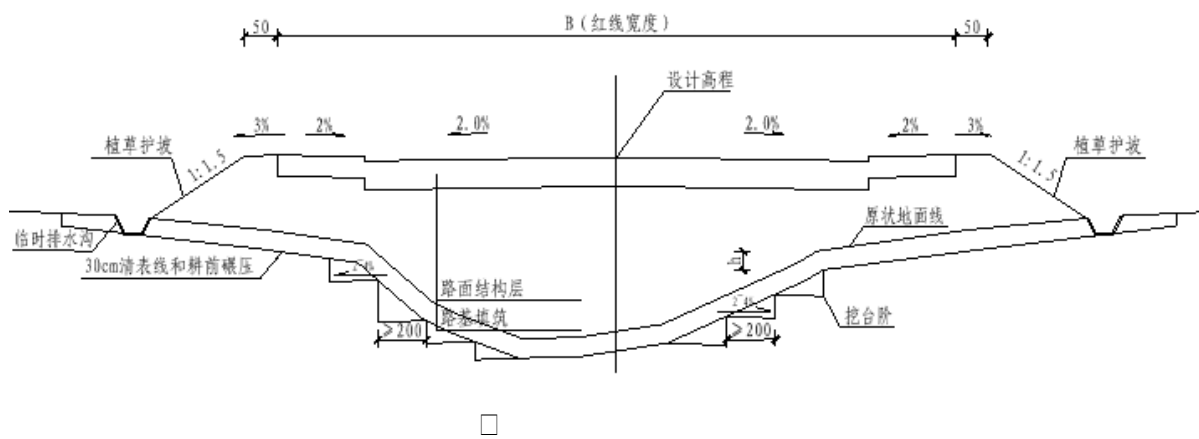
□

			hm <sup>2</sup>
		1819.09m	4.53
			4.53

□

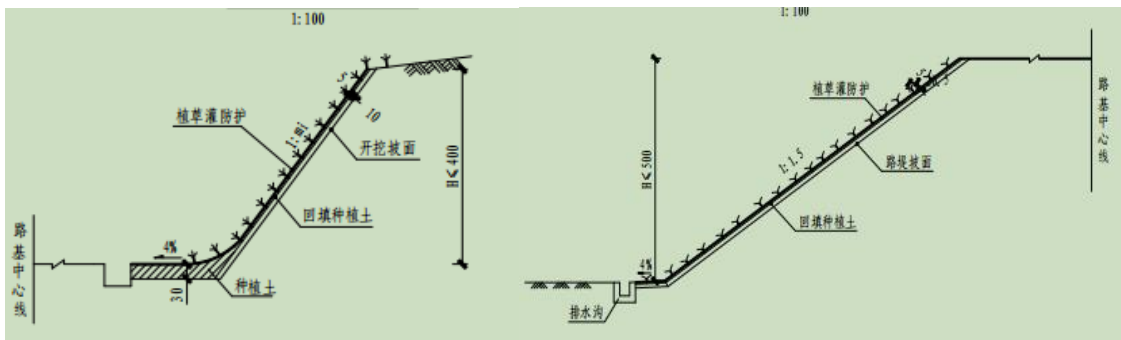












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10

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	m <sup>3</sup>		hm <sup>2</sup>	m	( m <sup>3</sup> )	m	
1	0.45		0.23	435.18~439.07	0.67	2	

□ □





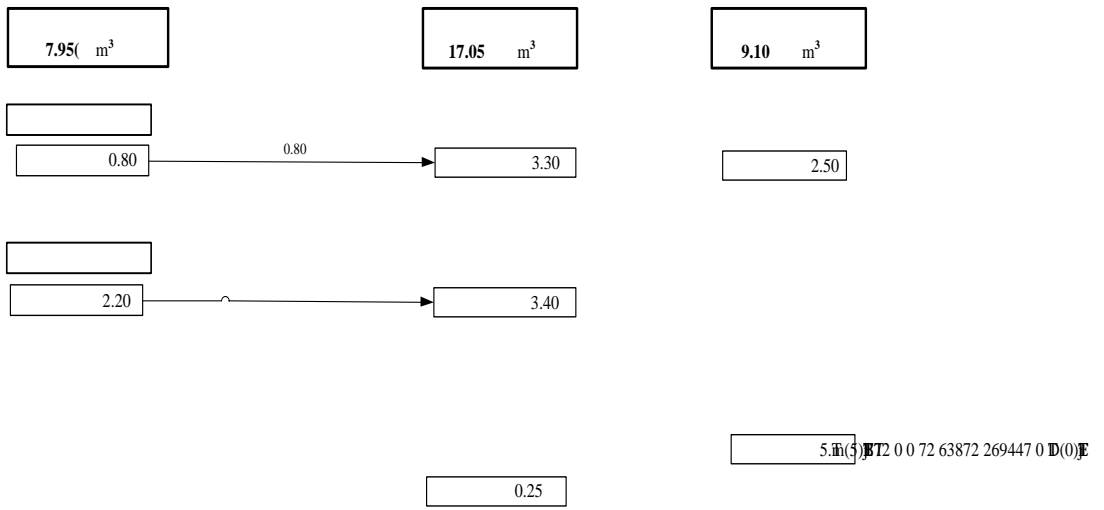
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□

		hm <sup>2</sup>	
		4.53	
		0.23	
		4.76	

□

□ □



2.4-1 ( m<sup>3</sup>)



□

□

2025 2

2024 5

2024 8 ~

2024 6 ~

2024 11 ~2025

□

	2024										2025	
	5	6	7	8	9	10	11	12	1	2		
1	■											
2		■	■	■	■							
3				■	■	■	■					
4								■	■	■		
5												■

□

□ □





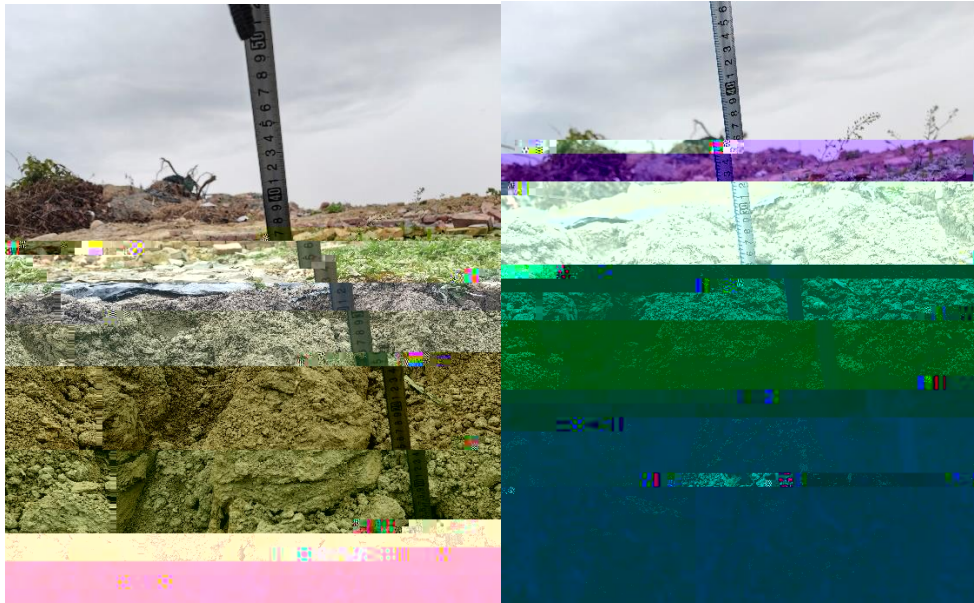
□ □

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			16.4
			38.2
			-7.3
			5212
	24h	mm	306.0
		/	1.1
		h	1306
			275
		%	78

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GB 50433-2018

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<b>1</b>		
<b>2</b> (		
<b>3</b>		

□ □

10

-

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□ □

1

2

1

2

□ □





$$C = R^{1/6} / n$$

$R$

$i$

□

	m <sup>3</sup> /s						C	m <sup>3</sup> /s
		b m	h m	A	X	R		
	0.04	0.24	0.24	0.06	0.72	0.09	74.06	0.10



□


□



			DN600	m	464	227	10.53
			DN300	m	829	119	9.87
					86	1478	12.71
			-		10709	43	46.05
			-	m	3326	27.33	9.09
			-		11484	154.83	177.81
					207	1196	24.76
					110	1896	20.86
			-		1	0.55	0.55
							595.91

□

□

		km <sup>2</sup>	km2				
	km2	95.42	69.74	19.78	4.38	1.52	0
	%		73.09	20.73	4.59	1.59	0.00

□

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		4.53	4.53
		0.23	0.23
		4.76	4.76

□

□ □

□ □

□

				a	
	hm <sup>2</sup>	hm <sup>2</sup>			
	4.53	1.15		0.8	2
	0.23	0.23		0.8	2
	4.76	1.38			

□ □

□

		hm <sup>2</sup>		%		t/km <sup>2</sup> a	t/a
		4.53	0 5			300	13.6
		0.23	0 5	30		300	0.69
		4.53				300	14.29

□ " □

	R		K		L	S	B	P	A	M
	MJ	mm/(hm <sup>2</sup> ·h)	t·hm <sup>2</sup>	h(hm <sup>2</sup> MJ mm)					t/hm <sup>2</sup> ·a	t/km <sup>2</sup> ·a
	4315.2		0.0070		0.61	4.97	0.39	1	35.71	3571
	4315.2		0.0070		0.58	4.95	0.38	1	32.95	3295

□ □ □

	R		K		L	S	B	P	A	M
	MJ	mm/(hm <sup>2</sup> ·h)	t·hm <sup>2</sup>	h(hm <sup>2</sup> MJ mm)					t/hm <sup>2</sup> ·a	t/km <sup>2</sup> ·a
	4315.2		0.007		0.61	4.97	0.08	1	7.33	733
	4315.2		0.007		0.61	4.97	0.04	1	3.66	366
	4315.2		0.007		0.58	4.95	0.06	1	5.20	520
	4315.2		0.007		0.58	4.95	0.02	1	1.73	173

□ □

$$W_1 = \sum_{i=1}^n \sum_{k=1}^3 F_{ik} \times M_{ik} \times T_{ik}$$

$$\Delta W = \sum_{i=1}^n \sum_{k=1}^3 F_{ik} \times \Delta M_{ik} \times T_{ik}$$

$$\Delta M_{ik} = \frac{(M_{ik} - M_{io}) + |M_{ik} - M_{io}|}{2}$$

## 4.3-5

		t/km <sup>2</sup> •a	t/km <sup>2</sup> •a	hm <sup>2</sup>	a	t	t	t
		300	3571	4.53	0.8	11.34	134.96	123.62
	1		733	1.15	1	0.00	8.41	8.41
	2		366	1.15	1	0.00	4.21	4.21
						11.34	147.58	136.24
		300	3295	0.23	0.8	0.58	6.32	5.74
	1		520	0.23	1	0.00	1.20	1.20
	2		173	0.23	1	0.00	0.40	0.40
						0.58	7.91	7.34
				4.76		11.91	141.28	129.36
				1.38		0.00	14.22	14.22
						11.91	155.49	143.58

□





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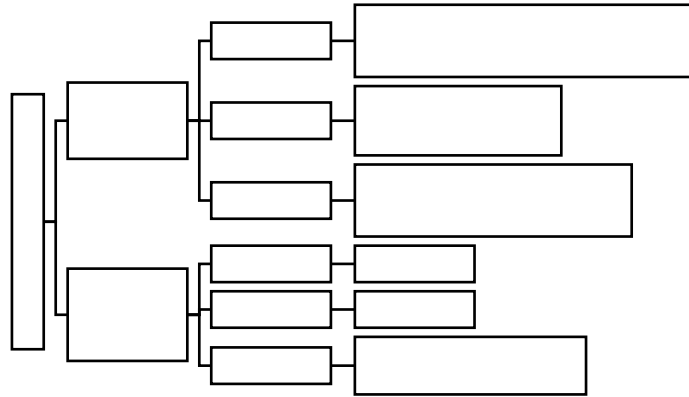
	4.53	
	0.23	
	4.76	

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□







			-	m <sup>3</sup>	4535	
			-	m <sup>3</sup>	4535	
			DN2000	m <sup>3</sup>	359	
			DN1800	m <sup>3</sup>	397	
			DN1600	m	285	
			DN1000	m	805	
			DN600	m	464	
			DN300	m	829	
					86	
			-		10709	
			-	m	3326	
			-		11484	
					207	
					110	
			-		1	
			-	m	3326	
			-		5	
					27207	



□

			-		2300	
			-		2300	
				m	114	
					2	
				m	68	
					2300	

□ □

□

			-	m <sup>3</sup>	4530	
			-	m <sup>3</sup>	4530	
			DN2000	m	359	
			DN1800	m	397	
			DN1600	m	285	
			DN1000	m	805	
			DN600	m	464	
			DN300	m	829	
					86	
			-		10709	
			-	m	3326	
			-		11484	
					207	
					110	
			-		1	
			-	m	3326	
			-		5	
				m <sup>2</sup>	27207	
			-	m <sup>2</sup>	2300	
			-	m <sup>2</sup>	2300	
			-	m	114	
			-		2	
			-	m	68	
				m <sup>2</sup>	2300	

□

							2024	2025
		-	m <sup>3</sup>	4530	4530	4530		
		-	m <sup>3</sup>	4530	4530	4530		
		DN2000	m	359	359	359		
		DN1800	m	397	397	397		
		DN1600	m	285	285	285		
		DN1000	m	805	805	805		
		DN600	m	464	464	464		
		DN300	m	829	829	829		
				86	86	86		
		-		10709	10709	10709		
		-	m	3326	3326	3326		
		-		11484	11484	5742	5742	
				207	207		207	
				110	110		110	
		-		1	1	1		
		-	m	3326	3326	3326		
		-		5	5	5		
			m2	27207	27207	21766	5441	
		-	m2	2300	2300		2300	
		-	m2	2300	2300		2300	
		-	m	114	114	114		
		-		2	2	2		
		-	m	68	68	68		
			m2	2300	2300	2300		

□

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□

			2024							2025				
			5	6	7	8	9	10	11	12	1	2		
			<hr/>											
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			<hr/>											
										---				

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$$A = ZS / 1000 \cos \theta$$

*A*

*Z*

*S*

*θ*



						2025 2 -2025 12 1 12h 50mm 1

□

□

1			1	
2			1	
3			1	
4	GPS		1	
5	2m		6	
6	50m		1	
7	5m		4	
8			1	
9	0.6cm		100	
10	1000ml		10	
11			6	
12				
13			1	
14			1	
15			1	
16			15	

□

				(	(
					236569
					16569
			1	4000	4000
			1	450	450
			1	1700	1700
	GPS		1	2200	2200
	2m		6	110	660
	50m		1	20	20
	5m		4	10	40
	1000ml		10	5	50
			6	9	54



□

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4

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			( )						
1			2.8	2.8					
2		t	7213.44	7213.44					
3			9.05	9.05					
4			1.04	1.04					
5			1.2	1.2					

□

1	37kw	50.59					
			3.04	3.65	0.16	7.67	36.06

□

		%	(%)	(%)	(%)	(%)
1		1	2.3	2.3	2.3	2.3
2		3.3	5.5	4.3	6.5	4.4
3		7	7	7	7	7
4		9	9	9	9	9



□

		371.95				371.95	371.92	0.02
			223.57			223.57	223.42	0.15
		37.26				37.26	0.55	36.71
					77.86	77.86		77.86
						35.53		35.53
						6.19		6.19
						752.36	595.89	156.47

□

						371.95	
		-	m <sup>3</sup>	4530	30.31	13.73	
		-	m <sup>3</sup>	4530	49.36	22.36	
		DN2000	m	359	2042	73.31	
		DN1800	m	397	1883	74.76	
		DN1600	m	285	1673	47.68	
		DN1000	m	805	644	51.84	
		DN600	m	464	227	10.53	

		DN300	m	829	119	9.87	
				86	1478	12.71	
		-		10709	43	46.05	
		-	m	3326	27.33	9.09	
		-	hm2	0.23	1057.66	0.02	
						223.57	
						223.42	
		-	m2	11484	154.83	177.81	
				207	1196	24.76	
				110	1896	20.86	
						0.15	
		-	hm2	0.23	6710.68	0.15	
						37.26	
						33.20	
		-		1	5500	0.55	
			m <sup>3</sup>	449.0	51.31	2.30	
				5221.8	16.49	8.61	
			m <sup>3</sup>	11.65	41.4	0.05	
				35.00	16.49	0.06	
				27207	6.3	17.14	
			m <sup>3</sup>	15.4	51.31	0.08	
				179.0	16.49	0.30	
			m <sup>3</sup>	4.66	41.4	0.02	
				14.00	16.49	0.02	
			m <sup>3</sup>	89	262.44	2.34	
			m <sup>3</sup>	89	32.01	0.29	
				2300	6.3	1.45	
						4.05	

632.78

		77.86	48.00	29.86
1		3.69	2.95	0.74
2		26.12	26.12	
3		0.00		
4		23.66	18.93	4.73
5		24.39		24.39
6		0.00	0.00	
7		0.00	0.00	
		35.53	35.53	
		6.19	6.19	
		752.36	562.02	190.34
□				
			77.86	

□

1		100m2	622.84	465.02	135.00	319.56		10.45	20.46	33.98		46.75	56.62
2		hm2	6710.68	5063.64	202.50	4811.01		50.14	167.10	366.15		503.72	610.06
3		hm2	1057.66	781.43	256.50	1.46	505.90	17.57	42.98	57.71		79.39	96.15
4	) (	100m3	5131.01	3755.35	3564.00	106.92		84.43	244.10	279.96		385.15	466.46
5	) (	100m3	4139.79	3029.89	2875.50	86.27		68.12	196.94	225.88		310.74	376.34
6		100m3	26243.58	19593.85	15687.00	3466.32		440.53	862.13	1431.92			

□

□

	4.53	4.53	4.53	2.32	1.07	1.15
	0.23	0.23	0.23			0.23
	4.76	4.76	4.76	2.33	1.07	1.36

\_\_\_\_\_

\_\_\_\_\_

□

	t/km a	hm <sup>2</sup>	t/a	t/km a	t/a	
	500	4.53	22.67	280	12.70	1.79
	0.23	500	1.15	280	0.64	1.79
	4.76	500	23.82	280	13.34	1.79

□

99.27

4.76

28.57

□

(%)		4.76hm <sup>2</sup>	100.00	97	
		4.76hm <sup>2</sup>			
		500	1.79	1.0	
		280			
(%)		13.81	99.64	93	
		13.86			
(%)		0.44	97.78	92	
		0.45			
(%)		1.36hm <sup>2</sup>	99.13	97	
		1.37hm <sup>2</sup>			
(%)		1.36hm <sup>2</sup>	25.39	25	
		4.76hm <sup>2</sup>			





